

Coupled Inductor Design of Interleaved CF-DAB Converter for Fuel Cell

with Maxwell analysis



Gyeongsang National University
Power Electronics and Motion Control Lab.

Jeong-In Lee

Outline

1. Introduction
2. Interleaved CF-DAB converter with coupled inductor
3. Coupled inductor design of interleaved CF-DAB converter
4. Maxwell analysis result
5. Conclusion

Introduction

❖ Fuel cell policy and market outlook

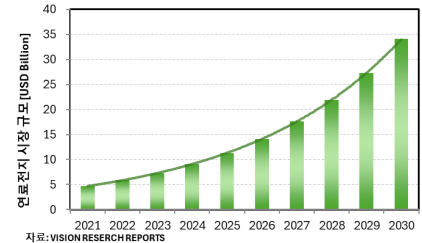
- Core technology for distributed/flexible power sources
- Continuous domestic policies related to hydrogen
- Global fuel cell market: \$2.62 billion as of 2020
- Korean fuel cell market: Cumulative installed capacity of 611,568 kW as of 2020
- Diversification of application fields such as ships and drones



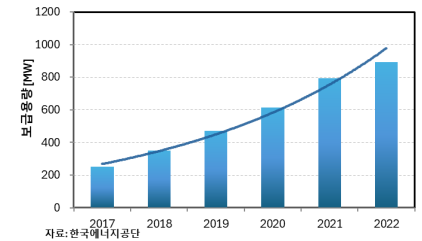
< Advantages of fuel cells >



< History of Korea's hydrogen policy >



< Global fuel cell market outlook >

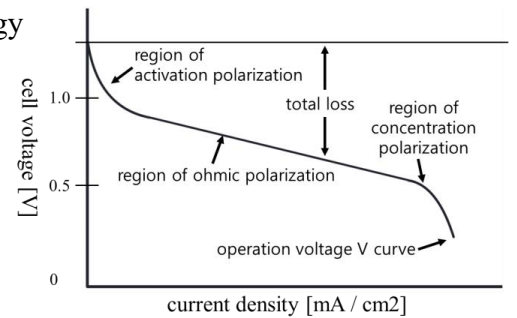


< Cumulative installed capacity of fuel cells(Korea) >

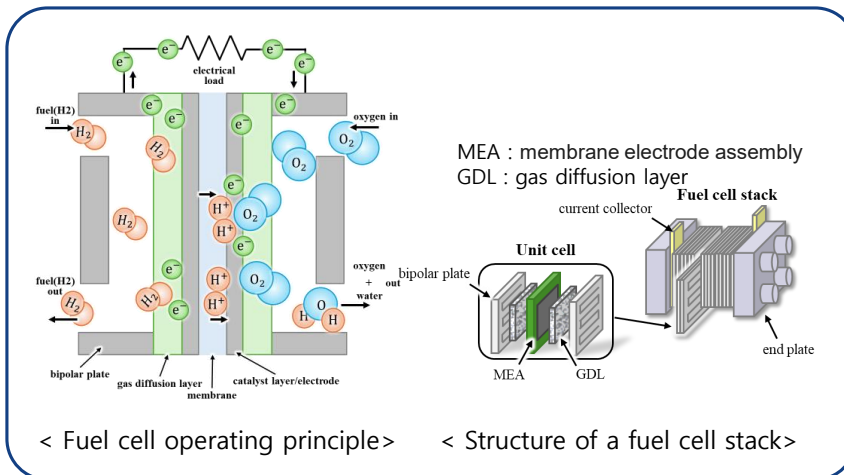
Introduction

❖ Fuel cell operating principles and electrical characteristics

- Converts chemical energy: Hydrogen&Oxygen → Electrical energy
- Stack output voltage drops with increased load
- Low voltage/High current
- Load current ripple → Adversely affects fuel cell stack lifespan

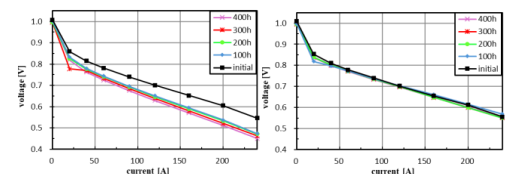


< I-V characteristic curve of fuel cell >



< Fuel cell operating principle >

< Structure of a fuel cell stack >



< Fuel Cell I-V Characteristic Curve >
(Left) Load variation, (Right) Constant current output

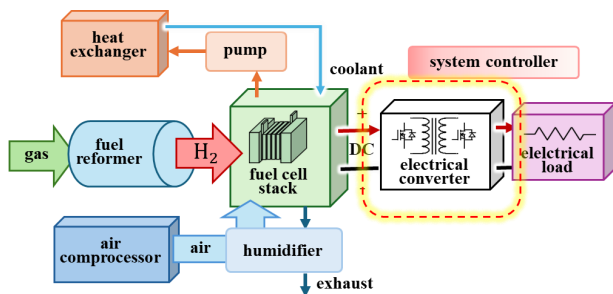
Introduction

❖ Components of the fuel cell system

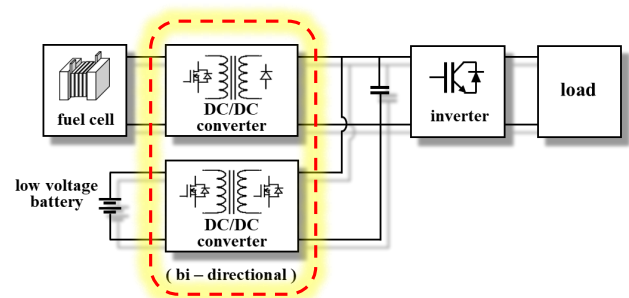
- Fuel cell stack, MBOP(Mechanical Balance of Plant), EBOP(Electrical Balance of Plant), control unit
- EBOP: Converts the electrical energy output of the fuel cell stack into form suitable for load requirements

❖ Evaluation criteria for DC-DC converter for fuel cell system

- High step-up and high efficiency
- Low input current ripple
- Wide input/output range



< Configurations of a Fuel cell system >

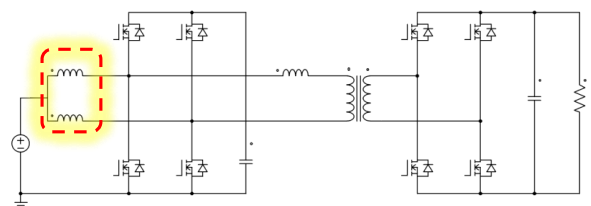


< Fuel cell and battery hybrid system EBOP configuration >

Introduction

❖ 2-phase interleaved CF-DAB(Current Fed Dual Active Bridge)

- Step-up topology; achieved high step-up
- Soft switching(ZVS) operation; achieved high efficiency
- Interleaving structure ; achieved low input current ripple
- Fuel cell application systems; low voltage/high current



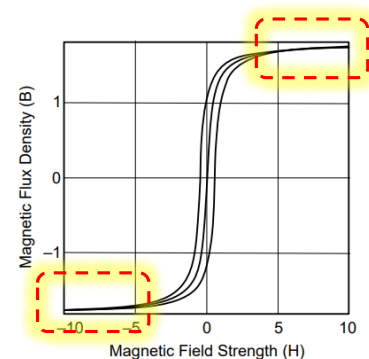
< 연료전지용 인터리브드 전류형 DAB 컨버터 >

❖ Design precautions for 2-phase interleaved CF-DAB

- Twice the number of components as single-phase
 - Increased system volume
- Low voltage/high current
 - **High risk of input inductor saturation**



When fabricating a 2-phase interleaved CF-DAB, pay close attention to **system size and input inductor saturation**



< 코어 B-H 곡선 >

- ❖ Research on existing coupled inductor-based DC-DC converters
 - Interleaved CF-DAB based on coupled inductor
 - ➔ Integrate the CF-DAB input inductor into a coupled inductor
 - ➔ Reduce the number of magnetic elements → Reduce system volume
 - Interleaved CF-DAB based on dual coupled inductor
 - ➔ Integrate two input inductors, a transformer, and leakage inductance into two EE cores
 - ➔ Reduce system volume due to reduced losses and fewer magnetic elements



- **No suitability evaluation as a coupling inductor of DC-DC converter for fuel cells**

- ❖ Mathematical modeling and design of coupled input inductor of interleaved CF-DAB
- ❖ Validation of the coupled input inductor design via Finite Element Analysis(FEA)
- ❖ Simulation analysis and validation of the interleaved CF-DAB converter with designed coupled inductor

Interleaved CF-DAB converter with coupled inductor

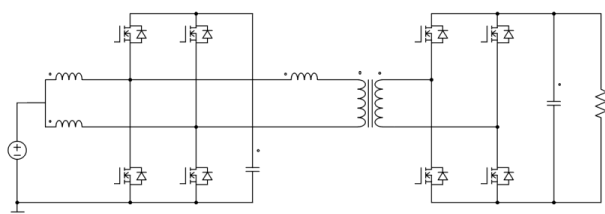
❖ Interleaved CF-DAB

- Interleaving operation with a 180-degree phase difference
- Output control; the phase difference between the two bridges
- Inductor current ripple in each phase cancels out
→ Low input current ripple
- Step-up converter capable of ZVS
→ High efficiency/High step-up

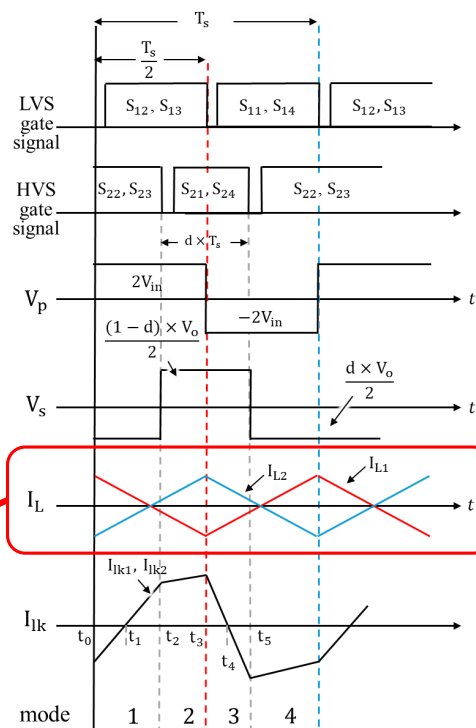
❖ Output equations

$$P_o = \frac{V_{in} V_o}{n f L_{lk}} \times \frac{\theta \cdot (\pi - \theta)}{\pi^2}$$

$$I_o = \frac{V_{in}}{n f L_{lk}} \times \frac{\theta \cdot (\pi - \theta)}{\pi^2}$$



<Interleaved CF-DAB>



Current ripple cancellation

<Main waveforms>

Interleaved CF-DAB converter with coupled inductor

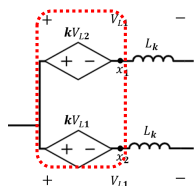
❖ Interleaved CF-DAB with coupled inductor

- 2 input inductors
→ changed to 1 coupled inductor with a 1:1 turn ratio

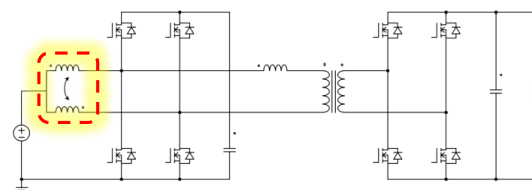
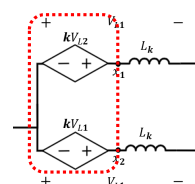
❖ Coupled inductor equivalent circuit

- Representing the coupled inductor
→ Dependent source and leakage inductance
- The direction of the dependent source varies

- Case 1: Directly coupled

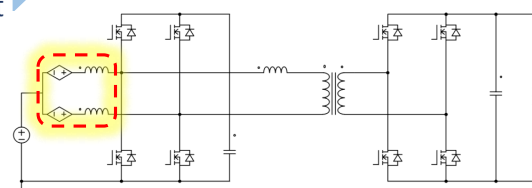


- Case 2: Indirectly coupled



<Interleaved CF-DAB with coupled inductor>

Equivalent circuit



<Coupled inductor equivalent circuit>

Interleaved CF-DAB converter with coupled inductor

❖ Comparison of characteristics based on coupling direction

	Directly coupled	Indirectly coupled
Equivalent circuit		
Features	<ul style="list-style-type: none"> - Alternating current component of the magnetic flux is canceled out - High efficiency by the core loss reduction - Core saturation risk increase 	<ul style="list-style-type: none"> - DC component of the magnetic flux is canceled out - Core weight reduction by the core saturation risk decrease - High current ripple increase
Total magnetic flux Φ_m	$\Phi_m = \Phi_{21} + \Phi_{12}$	$\Phi_m = \Phi_{21} - \Phi_{12}$
Current ripple slope S of each phase inductor	$S = \frac{V_{in} - kV_{L2} - V_{L1}}{L_{lk}}$	$S = \frac{V_{in} + kV_{L2} - V_{L1}}{L_{lk}}$

Interleaved CF-DAB converter with coupled inductor

❖ Interleaved CF-DAB with indirect coupled inductor

□ Current ripple $\Delta I_L, \Delta I_{in}$

$$- \Delta I_L = \frac{(1-k \cdot d_{LV} / (1-d_{LV})) V_{in}}{L_{lk}} \times d_{LV} T_s$$

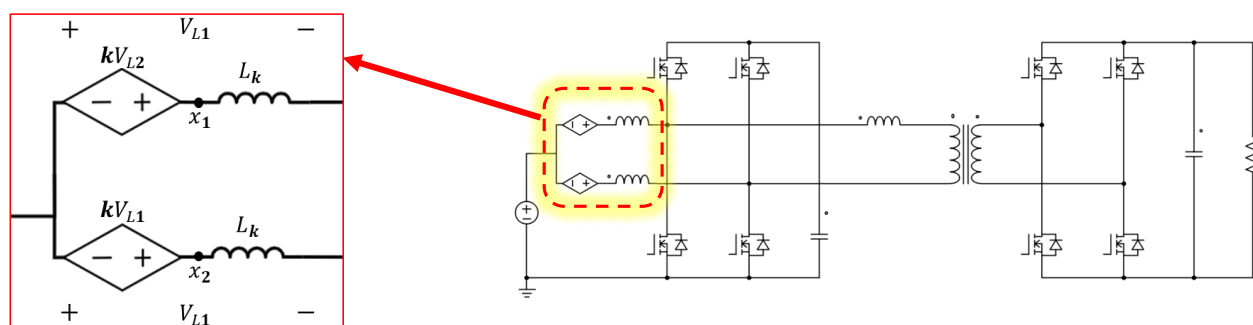
$$- \Delta I_{in} = \frac{2(1+k) d_{LV} V_{in}}{(1-d_{LV}) L_{lk}} \times (0.5 - d_{LV}) T_s$$

LV-side duty $d_{LV} = 0.5$



$$- \Delta I_L = \frac{(1-k) V_{in}}{L_{lk}} \times \frac{T_s}{2}$$

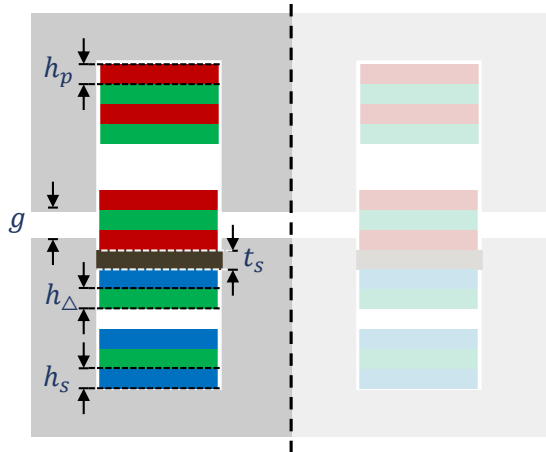
$$- \Delta I_{in} = 0$$



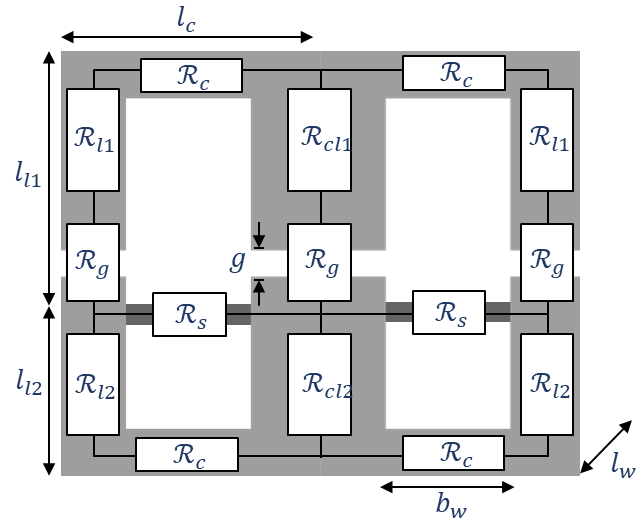
Coupled inductor design of interleaved CF-DAB converter

❖ Planar coupled inductor

- Configuration : Type E ferrite core, primary and secondary PCB windings, magnetic sheet
- Insertion of magnetic sheet between primary and secondary windings → High leakage inductance
- Sufficient inter-winding spacing → Copper losses due to proximity effects negligible
- Small volume**
- High reproducibility** → Suitable for interleaved converter requiring identical specifications



<Planar coupled inductor structure>



<Planar coupled inductor magnetic circuit>

Coupled inductor design of interleaved CF-DAB converter

❖ Inductance of planar coupled inductor

- $L_m = \frac{N^2}{\mathcal{R}_1} \parallel \left(L_{lk} + \frac{N^2}{\mathcal{R}_2} \right) - \left(\frac{N^2}{\mathcal{R}_1} \parallel L_{lk} \right) \cong \frac{N^2}{\mathcal{R}_1} - \left(\frac{N^2}{\mathcal{R}_1} \parallel L_{lk} \right)$
- $L_{lk} = L_{ksh} + L_{kw} \cong L_{ksh}$
- $L_{ksh} = 2\mu_0\mu_r \times \frac{F_s^2 A_s}{I_1^2 b_w}$

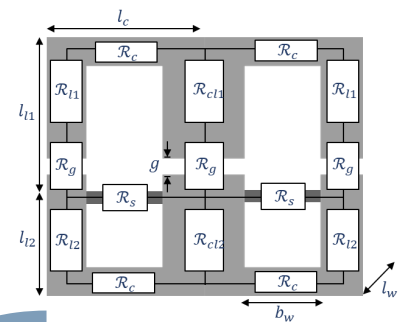
❖ Reluctance calculation

- $\mathcal{R}_1 = \frac{2g}{\mu_0 A_g} + \frac{l_1}{\mu_0 \mu_r A_c}$
- $\mathcal{R}_2 = \frac{l_2}{\mu_0 \mu_r A_c}$
- $\mathcal{R}_s = \frac{b_w}{\mu_0 \mu_s A_s} = \frac{b_w}{\mu_0 \mu_r l_w t_s}$
- $l_1 = l_c + 2l_{l1}$
- $l_2 = l_c + 2l_{l2}$

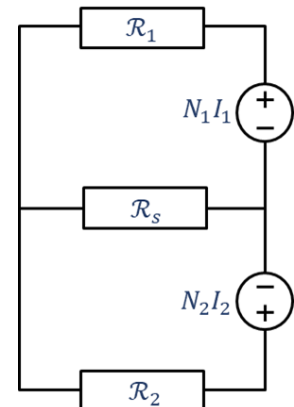
L_{ksh} : Leakage inductance due to magnetic sheet

L_{kw} : Leakage inductance from windings and insulator

N : Inductor turns



Equivalent circuit

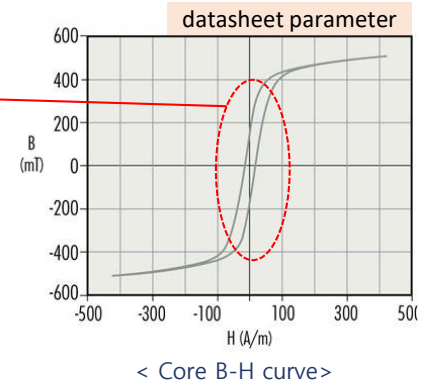


<Magnetic equivalent circuit>

Coupled inductor design of interleaved CF-DAB converter

❖ Saturation of the magnetic core

- $\Phi_{sat} = A_c \times B_{sat}$
- $I_{sat} = \frac{NA_c}{L_m} \times B_{sat}$



❖ Magnetic design of a indirectly coupled inductor

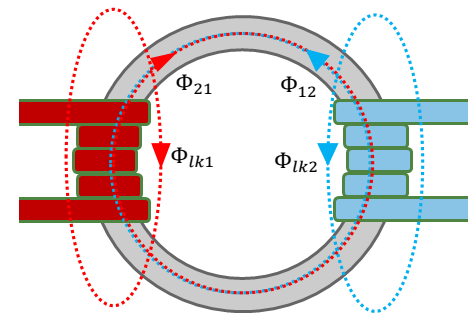
- $\Phi_m = \Phi_{21} - \Phi_{12}$
 → Where, since the MMF of the two winding ar the same
 → $\Phi_{21} = \Phi_{12}$
 → Thus, $\Phi_m = 0$

- Magnetic field strength H
 → $H_{max} = 2 \cdot \pi \cdot \frac{N \cdot \Delta i_L}{l_e}$
 → $H_{min} = -2 \cdot \pi \cdot \frac{N \cdot \Delta i_L}{l_e}$

Φ_{sat} : Core saturation magnetic flux

I_{sat} : Core saturation current

B_{sat} : Core saturation magnetic flux density



< Core flux flow diagram >

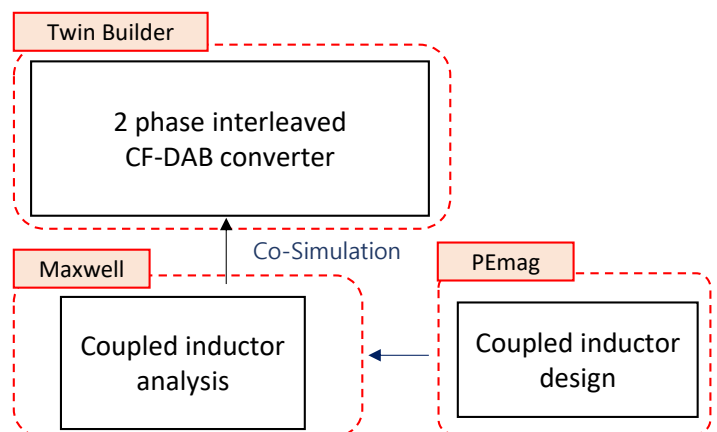
Maxwell analysis result

❖ Ansys/Maxwell

- Finite Element Analysis (FEA)
- Co-simulation analysis

❖ Evaluation indicators

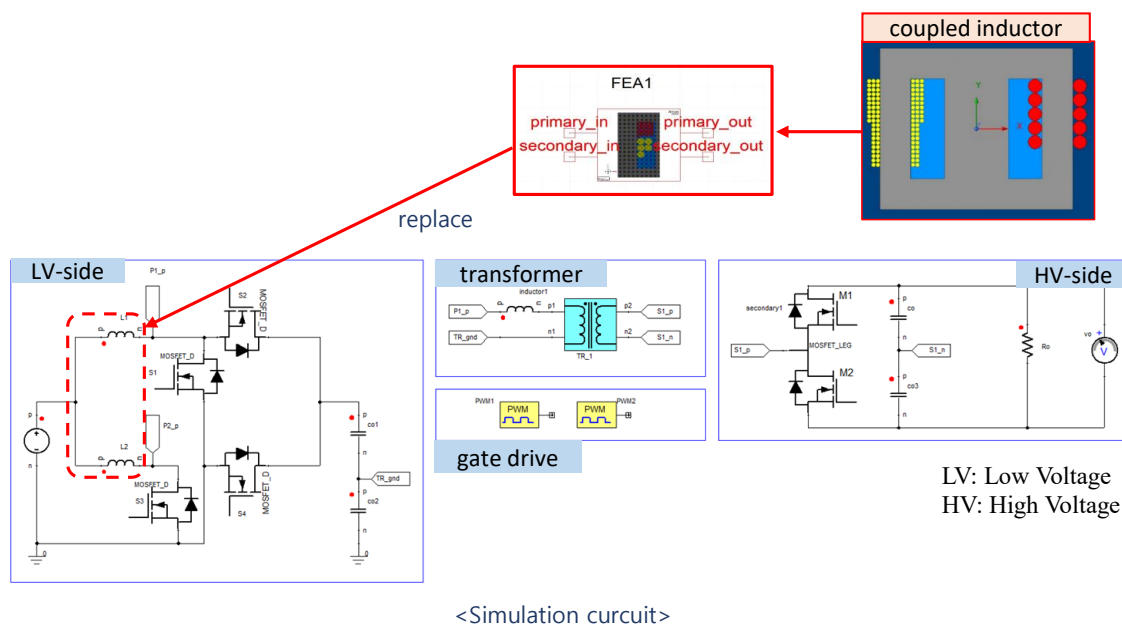
- Inductor flux density
- Input current ripple and phase current ripple
- Converter input/output voltage/current



Maxwell analysis result

❖ Simulation specifications

- 2-Phase interleaved CF-DAB converter
- 1kW, input voltage: 50V → output voltage: 300V
- Modeling with Ansys/Maxwell
 - 2-Phase CF-DAB simulation via Co-Simulation



Maxwell analysis result

❖ Inductor specifications

Item	Saparated inductors	Coupled inductor	
Core	0077439A7	CR45810EC	
Input inductance	108.2uH	108.6uH	k = 0.85
Turns	31 turn	10 turn	
Magnetic sheet	-	EFW-02-240X80-T0800	
I_{sat}	15 A	15 A	

- ❖ Presentation of mathematical modeling/design of the coupled inductor for the interleaved CF-DAB converter
- ❖ Verification of feasibility as the MBOP for fuel cells through Maxwell simulation analysis
- ❖ Future review of validity through prototype fabrication and experimentation

Thank you for your attentions

THANK YOU FOR YOUR ATTENTIONS

Any Questions?